

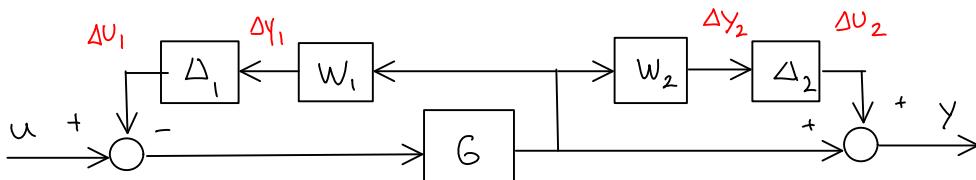
## MIMO uncertainty and Robustness

A couple of factors that differentiate the MIMO case from SISO case :

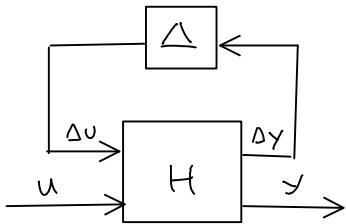
- Structure of uncertainty
- Input and output uncertainty

### Structure of uncertainty

Consider the example :



We can lump the uncertainties as :



$$\text{where } \Delta(s) = \begin{bmatrix} \Delta_1(s) & 0 \\ 0 & \Delta_2(s) \end{bmatrix}$$

Observe that  $\|\Delta_1\|_\infty \leq 1, \|\Delta_2\|_\infty \leq 1 \Leftrightarrow \|\Delta\|_\infty \leq 1$

$\Delta(s)$  is a  $2 \times 2$  system. However it is structured as a diagonal system. If we ignore this constrained structure, we could get conservative result in robustness analysis.

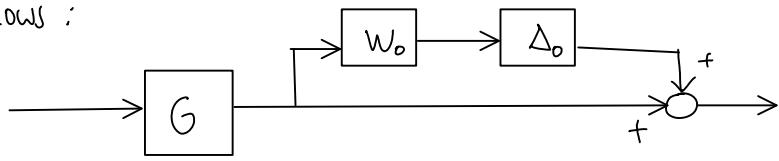
The term unstructured uncertainty refers to the uncertainty block  $\Delta(s)$  with only  $\|\Delta\|_\infty \leq 1$  constraint.

### Input and Output uncertainty

because transfer matrix multiplications generally do not commute, we have e.g.

$$G(\underbrace{I + W\Delta}_{\text{input}}) \neq (\underbrace{I + W\Delta}_{\text{output}}) G$$

Output side uncertainty can be modeled as unstructured uncertainty as follows :



$$G_p(s) = (I + W_0(s) \Delta_0(s)) G(s), \text{ where } W_0(s) \text{ is scalar and } \| \Delta_0 \|_\infty \leq 1$$

The weight  $W_0(s)$  can be constructed as follows :

$$\forall \omega \in \mathbb{R}, |W_0(j\omega)| \geq \Gamma_{\max} \left[ (G_p(j\omega) - G(j\omega)) G^{-1}(j\omega) \right]$$

Similarly, on the input side :

$$G_p(s) = G(s) (I + W_I(s) \Delta_I(s)), \text{ where } W_I(s) \text{ is a scalar and } \| \Delta_I \|_\infty \leq 1$$

The weight  $W_I(s)$  can be constructed as follows :

$$\forall \omega \in \mathbb{R}, |W_I(j\omega)| \geq \Gamma_{\max} \left[ G^{-1}(j\omega) (G_p(j\omega) - G(j\omega)) \right]$$

If  $G(j\omega)$  is not invertible, then we can use pseudo inverse. Note that there are geometric considerations.

Ex: Given a  $1 \times 2$  plant with uncertainty :

$$G_p(s) = \begin{bmatrix} G_1(s) (I + W_1(s) \Delta_1(s)) & G_2(s) (I + W_2(s) \Delta_2(s)) \end{bmatrix}$$

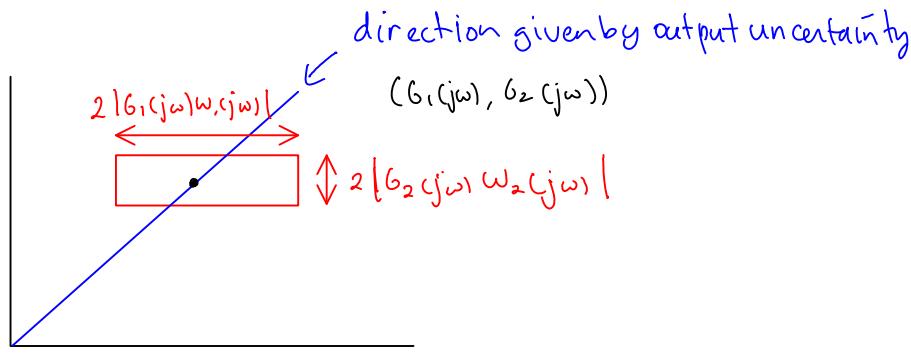
To model it as output side uncertainty, we have :

$$G_p(s) = (I + W_0(s) \Delta_0(s)) \underbrace{\begin{bmatrix} G_1(s) & G_2(s) \end{bmatrix}}_{G(j\omega)}$$

Thus, at every  $\omega$ ,

$$(G_p(j\omega) - G(j\omega)) = \underbrace{W_0(j\omega) \Delta_0(j\omega)}_{1 \times 1 \text{ transfer function}} G(j\omega)$$

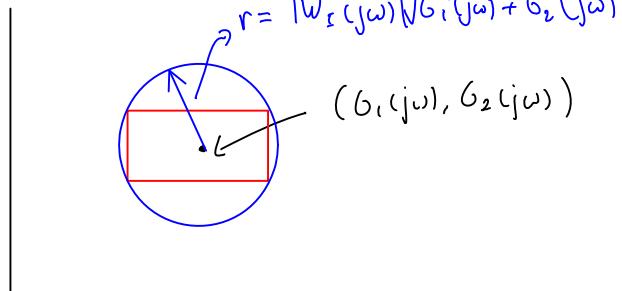
Illustration:-



On the other hand, if we model it as unstructured input uncertainty:

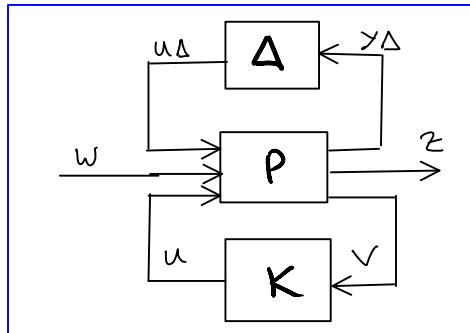
$$G_p(s) = [G_1(s) \quad G_2(s)] \cdot (I + W_I(s) \Delta_I(s))$$

$$\text{Hence, } (G_p(j\omega) - G(j\omega)) = W_I(j\omega) \cdot [G_1(j\omega) \quad G_2(j\omega)] \begin{bmatrix} \Delta_{11}(j\omega) & \Delta_{12}(j\omega) \\ \Delta_{21}(j\omega) & \Delta_{22}(j\omega) \end{bmatrix}$$

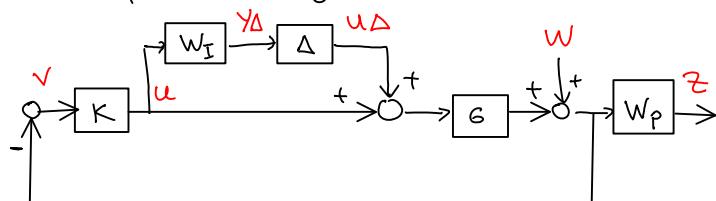


Thus, input side uncertainty can capture the uncertainty with some conservativeness

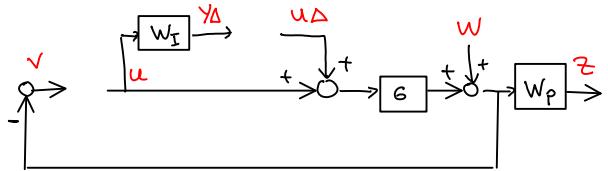
### General Control Problem Formulation:



Example : See Fig 8.7 in text book



General Plant model :  $\begin{bmatrix} Y_\Delta \\ z \\ v \end{bmatrix} = \begin{bmatrix} P_{11} & P_{12} & P_{13} \\ P_{21} & P_{22} & P_{23} \\ P_{31} & P_{32} & P_{33} \end{bmatrix} \begin{bmatrix} u^\Delta \\ w \\ u \end{bmatrix}$



$$\left. \begin{array}{l} Y_\Delta = w_I u \\ z = w_p (w + Gu + Gu\Delta) \\ v = -(w + Gu + Gu\Delta) \end{array} \right\} P = \begin{bmatrix} 0 & 0 & w_I \\ w_p G & w_p & w_p G \\ -G & -I & -G \end{bmatrix}$$

Once we have a controller, the lower loop can be closed to assess robustness properties. Use the lower LFT

$$P_{11} \triangleq \begin{bmatrix} 0 & 0 \\ w_p G & w_p \end{bmatrix}; P_{12} \triangleq \begin{bmatrix} w_I \\ w_p G \end{bmatrix}; P_{21} = [-G \quad -I]; P_{22} = -G$$

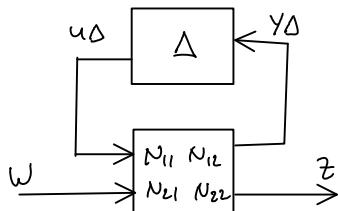
$$F_L(P, K) = P_{11} + P_{12} K (I - P_{22} K)^{-1} P_{21} \triangleq N$$

$$N = \begin{bmatrix} 0 & 0 \\ w_p G & w_p \end{bmatrix} + \begin{bmatrix} w_I \\ w_p G \end{bmatrix} K (I + GK)^{-1} [-G \quad -I]$$

$$N = \begin{bmatrix} -W_I K (I + GK)^{-1} G & -W_I K (I + GK)^{-1} \\ W_p G - W_p G K (I + GK)^{-1} G & W_p - W_p G K (I + GK)^{-1} \end{bmatrix}$$

$$N = \begin{bmatrix} -W_I K G (I + KG)^{-1} & -W_I K (I + GK)^{-1} \\ W_p G (I - KG (I + KG)^{-1}) & W_p (I - G K (I + GK)^{-1}) \end{bmatrix}$$

$$N = \begin{bmatrix} -W_I K G (I + KG)^{-1} & -W_I K (I + GK)^{-1} \\ W_p G (I + KG)^{-1} & W_p (I + GK)^{-1} \end{bmatrix}$$



Recall that good performance is characterized by the transfer function from  $w$  to  $z$  being small.

In this setup:

Nominal Stability :  $N$  is internally stable

Nominal Performance :  $\|N_{22}\|_\infty < 1$ , and NS

### Robust Stability & Robust Performance

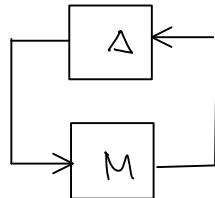
For any  $\Delta$ , if we close the upper loop (using upper LFT), we get the TF from  $w$  to  $z$ :

$$F \triangleq F_u(N, \Delta) = N_{22} + N_{21} \Delta (I - N_{11} \Delta)^{-1} N_{12}$$

If the system is nominally stable, to check robust stability we only need to make sure that

$$(I - N_{11} \Delta)^{-1} \text{ is stable}$$

In the book,  $N_{11}$  is called  $M$ , thus:



needs to be stable

for any  $\|\Delta\|_\infty \leq 1$

For robust performance:  $\|F\|_\infty < 1$  for all  $\|\Delta\|_\infty \leq 1$ , and NS